

Table II. Smoothed Values of Composition of Three-Phase Region

Press., Atm.	Temp., ° C.	Mole Fraction Ethane		
		Comp., liquid 1	Comp., liquid 2	Comp., vapor phase
7.18	-40.00	0.360	0.957	0.992
10	-30.07	0.376	0.936	0.991
20	-5.65	0.410	0.934	0.990
30	10.80	0.357	0.936	0.989
40	23.78	0.354	0.941	0.988
50	35.25	0.348	0.962	0.986
51.08 <sup>a</sup>	36.42	0.351	0.979	0.979

<sup>a</sup> Critical temperature and pressure of the liquid 2 and vapor phase.

the equilibrium properties at these states are regarded as identical to those of pure ethane.

The smoothed three-phase data ( $L_1$ - $L_2$ - $V$ ) are shown at even pressures in Table II. In comparing those smoothed values presented in Table II with values of Kuenen (5), the average deviation of the pressure is 1% for temperatures below the critical point. At the critical point, the deviation is 3% and -3% in temperature and pressure, respectively. Kuenen's system contained air, which raised the critical pressure and lowered the critical temperature of the system.

From the compositions along the three-phase line given in Table II and illustrated by the dashed lines in Figure 1, there definitely does not seem to be a lower critical solution point for the system ( $L_1 = L_2$  in the presence of a vapor phase). Rather it would appear that at a temperature in the region of -97.8° C. that the three-phase line terminates at a quadruple point. At this point solid methanol should be in equilibrium with the ( $L_1$ ), ( $L_2$ ) and vapor phases.

## NOMENCLATURE

$L_1$  = liquid phase rich in methanol

$L_2$  = liquid phase rich in ethane

$V$  = vapor phase

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# Multiphase and Volumetric Equilibria of the Methane-*n*-Octane System at Temperatures between -110° and 150° C.

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Vapor-liquid compositions and molar volumes were determined at eight temperatures between -50° and 150° C. Temperature, pressures, and compositions along the three phase (vapor-liquid-solid) lines are reported at temperatures between -107.6° and -56.7° C.

THIS STUDY was undertaken in view of the scarcity of information on the low temperature phase and volumetric behavior of the methane-*n*-octane system. Such information is desirable for its use in low temperature theoretical studies and for its value in assessing the economic feasibility of employing low temperature separation processes in systems involving light hydrocarbon mixtures.

No studies of the vapor-liquid behavior of the methane-*n*-octane system were found in the literature. Brewer (1) reported a study of the three phase (solid-liquid-vapor) locus and reported compositions of the liquid phase.

The  $P$ - $V$ - $T$  behavior of the pure components has been studied. Methane has been investigated by several groups of investigators (3, 6, 8, 9, 10). Matthews (7) evaluated the thermodynamic properties of methane from selected  $P$ - $V$ - $T$  data previously mentioned.

Young (15, 16) presented vapor pressures, specific volumes, and critical constants of *n*-octane from -3° to 296° C. Felsing (2) reported the compressibility of liquid *n*-octane at temperatures from 100° to 275° C. at pressures to 300 atm. Data on the liquid density, vapor pressures, critical constants, and heat of fusion of *n*-octane were

reported by Rossini (12). Sage (13) summarized the *P-V-T-X* work done on the light hydrocarbon pure component, binary, and ternary systems to the year 1950.

## EXPERIMENTAL

The equipment and the experimental techniques were described by Kohn (5) and were the same as those used in other studies on binary hydrocarbon systems (4, 14).

The methane and *n*-octane were obtained from the Phillips Petroleum Co. Both components were "pure grade" materials stated to have 99% minimum purity. The methane was processed as described by Kohn and the resulting gas used in the study was thought to have a purity in excess of 99.5%. The *n*-octane was de-aerated before each experimental run and used without further purification.

## RESULTS

Eight experimental bubble point isotherms were determined for the range  $-57.22^{\circ}\text{C.}$  to  $150^{\circ}\text{C.}$  Each isotherm was run in a small borosilicate glass equilibrium cell of 5 cc. volume and in a large borosilicate glass cell of 12 cc. volume at pressures to 70 atm. The average deviation of the experimental bubble points was  $\pm 0.0015$  mole fraction,  $\pm 0.07^{\circ}\text{C.}$  and  $\pm 0.10$  atm.

Four experimental dew point isotherms were determined between  $25^{\circ}\text{C.}$  and  $150^{\circ}\text{C.}$  and at pressures to 70 atm. in a borosilicate glass equilibrium cell of 10 cc. volume. The dew point isotherms were run at least twice at each temperature with good reproducibility. At temperatures of  $150^{\circ}$  and  $100^{\circ}\text{C.}$ , the average deviation of the experimental points was  $\pm 0.002$  mole fraction,  $\pm 0.07^{\circ}\text{C.}$  and  $\pm 0.1$  atm. At  $50^{\circ}$  and  $25^{\circ}\text{C.}$ , the average deviation of the experimental points was  $\pm 0.001$  mole fraction,  $\pm 0.07^{\circ}\text{C.}$  and  $\pm 0.07$  atm. Vapor-liquid critical points were determined at  $25^{\circ}$  and  $50^{\circ}\text{C.}$  in a stainless steel equilibrium cell. Since these critical points were determined by graphical discontinuities in the mass *vs.* pressure relationships, they represent data of lower accuracy than that obtained in the borosilicate glass cells. The probable accuracy of the vapor-liquid critical points is  $\pm 0.07^{\circ}\text{C.}$ ,  $\pm 6$  atm. and  $\pm 0.02$  mole fraction.

Table I presents the smoothed *P-V-T-X* properties in the vapor-liquid region at temperatures between  $-50^{\circ}$  and  $150^{\circ}\text{C.}$  The saturated vapor properties were not measured below  $25^{\circ}\text{C.}$  because of the difficulty of accurately measuring concentrations of *n*-octane less than a few tenths of a mole per cent. The vapor volumes at  $25^{\circ}\text{C.}$  and above are reproducible to  $\pm 0.5\%$ . The liquid molar volumes are reproducible to  $\pm 0.1\%$ . The dew point composition were smoothed by use of the following thermodynamic equation:

Table I. Properties of the Coexisting Vapor and Liquid Phases

Pressure, Atm.	Liquid		Vapor <sup>a</sup>		Pressure, Atm.	Liquid		Vapor <sup>a</sup>	
	Mole fraction, methane	Molar volume, ml./gram mole	Mole fraction, methane	Molar volume, ml./gram mole		Mole fraction, methane	Molar volume, ml./gram mole	Mole fraction, methane	Molar volume, ml./gram mole
T = 150° C.					T = 25° C.				
1.995 <sup>b</sup>	0.000	193.8			0.020 <sup>b</sup>	0.000	163.5		
10	0.028	189.9		1708	10	0.047	158.2	0.998	2385
20	0.063	185.8	0.881		20	0.094	153.0	0.999	1167
30	0.097	181.5	0.914	1133	30	0.136	148.5	0.999	763.2
40	0.131	177.5	0.930	846.4	40	0.178	143.4	0.999	562.7
50	0.164	173.6	0.939	675.7	50	0.220	138.7	0.999	442.8
60	0.196	170.0	0.945	562.5	60	0.255	134.9	0.999	362.5
70	0.229	166.3	0.949	481.6	70	0.287	131.4	0.999	305.1
T = 100° C.					263 <sup>c</sup>	0.798	81.5	0.798	81.5
T = 75° C.					T = 0° C.				
0.463 <sup>b</sup>	0.000	179.6				0.000	158.9		
10	0.033	175.6	0.947	3034	10	0.054	153.0		
20	0.069	171.3	0.971	1505	20	0.106	147.4		
30	0.104	167.0	0.979	996.2	30	0.155	142.2		
40	0.139	162.8	0.982	742.5	40	0.201	137.2		
50	0.173	158.6	0.984	590.3	50	0.244	132.5		
60	0.207	154.5	0.985	488.9	60	0.285	128.0		
70	0.240	150.1	0.986	416.9	70	0.319	124.3		
T = 50° C.					T = -25° C.				
0.186 <sup>b</sup>	0.000	173.9				0.000	154.6		
10	0.038	169.0		2820	10	0.065	147.7		
20	0.075	165.0	0.985	1395	20	0.128	140.6		
30	0.112	160.6	0.990	920.8	30	0.187	134.4		
40	0.148	156.5	0.992	682.1	40	0.238	128.9		
50	0.183	152.5	0.993	540.5	50	0.288	123.6		
60	0.218	148.5	0.994	446.6	60	0.337	118.2		
70	0.251	144.8	0.994	379.5	70	0.373	114.1		
T = -50° C.					T = -50° C.				
0.065 <sup>b</sup>	0.000	168.4				0.000	150.5		
10	0.043	162.8	0.991	2604	10	0.086	141.4		
20	0.083	158.2	0.995	1281	20	0.168	132.5		
30	0.122	154.1	0.996	841.5	30	0.244	124.4		
40	0.161	149.8	0.997	622.5	40	0.312	117.0		
50	0.188	145.6	0.997	491.6	50	0.370	110.6		
60	0.234	141.8	0.997	404.8	60	0.424	105.0		
70	0.265	138.0	0.997	342.8	70	0.472	100.0		
269.8 <sup>c</sup>	0.787	86.1	0.787	86.1					

<sup>a</sup> Vapor compositions and molar volumes at  $0^{\circ}\text{C.}$  and lower temperatures are accurately given by properties of pure methane.

<sup>b</sup> Vapor pressure of pure *n*-octane. <sup>c</sup> Vapor-liquid critical state.

$$Y_1 = \frac{x_1 \gamma_1 \nu_{P_1} P_1}{\nu_P P} \exp \left[ \frac{V}{RT} (P - P_1) \right]$$

The activity coefficient was combined with the fugacity-coefficient ratio to give an empirical function of the reduced temperature and pressure of the *n*-octane. The resulting function is

$$\frac{\gamma_1 \nu_{P_1}}{\nu_P} = \exp \left[ A \frac{P_r^a}{T^b} \right]$$

The constants determined from the experimental data were  $A = 0.09$ ,  $a = 1.0$ ,  $b = 2.0$ . The equation with the constants given agrees with the experimental data of this study within  $\pm 0.003$  mole fraction at temperatures above  $100^\circ\text{C}$ . and within  $\pm 0.001$  mole fraction below  $100^\circ\text{C}$ . at pressures to 70 atm.

Table II presents data along the solid-liquid-vapor, three-phase lines. The air-saturated freezing point of *n*-octane reported here is within  $0.06^\circ\text{C}$ . of that reported by Rossini (12). The measured experimental solubility points were used to calculate the heat of fusion of *n*-octane from the Van't Hoff isochore. The calculated heat of fusion was  $4953 \pm 60$  cal. per gram mole which agrees with the literature value of 4957 cal. per gram mole (12). Because the Van't Hoff isochore regarding  $\Delta H_f$  as constant does not allow accurate calculation of the solubility of methane in *n*-octane in excess of 0.20 mole fraction, Raoult's law does not hold accurately for *n*-octane past 0.20 mole fraction methane. This was definitely demonstrated by the results of the low temperature vapor-liquid equilibrium study which showed that methane solubility up to about 0.20 mole fraction accurately followed Henry's law.

Table II. Smoothed Solid-Liquid-Vapor, Three-Phase Lines

Pressure, Atm.	Temperature, $^\circ\text{C}$ .	Liquid Phase Comp., Mole Fraction Methane	
		Exptl.	Calcd. <sup>a</sup>
1 atm. <sup>b</sup>	-56.73	0	0
5.20	-57.77	0.05	0.05
10.25	-58.75	0.10	0.10
20.60	-60.71	0.20	0.192
31.25	-62.67	0.30	0.275
43.20	-64.62	0.40	0.352
57.30	-66.56	0.50	0.420
70.50	-67.65	0.56	0.454
46.07	-82.46 <sup>c</sup>		
45.00	-83.21 <sup>b</sup>		
40.00	-88.80		
35.00	-91.30		
30.00	-96.10		
25.00	-101.50		
20.00	-107.60		

<sup>a</sup> Calculated from simple Van't Hoff isochore regarding  $\Delta H_f = (H_L - H_S) = 4953$  cal./gram mole. <sup>b</sup> Air-saturated freezing point. <sup>c</sup> Type *k* singular point. (Vapor is identical with the liquid in the presence of the solid phase.)

The three-phase, solid-liquid-vapor line, which is actually a three-phase surface in three dimensions intersects the vapor-liquid critical locus. This was positively shown by the observation of a type-*k* singular point at  $-82.46^\circ\text{C}$ . and 46.07 atm. At this point, the vapor phase is in critical identity with the liquid phase in the presence of the solid phase. The singular point is quite close in temperature and pressure to the critical point of pure methane. The three-phase, solid-liquid-vapor line below  $-82.46^\circ\text{C}$ . appears to parallel the vapor pressure curve of pure methane. The equilibrium pressures average about 0.5 atm. higher than those of pure methane when measured at the same

temperature. This effect may result from using values of the vapor pressures of methane which have never been measured accurately. The small deviation in the vapor pressure of methane indicates that the composition of both the liquid and the vapor phases is reasonably pure methane.

There are two separate type-*k* singular points in this system. The second one was not found because of the pressure limitation of the borosilicate glass cells. All evidence would indicate that this point should be found at pressures in excess of 100 atm. and temperatures between  $-70^\circ$  and  $-80^\circ\text{C}$ . The extrapolated value of the second type-*k* point is 200 atm.,  $-72^\circ\text{C}$ . and 0.90 mole fraction methane.

The higher temperature solid-liquid-vapor line was compared with that of Papahronis (11) which was reported by Brewer (1). Papahronis' three-phase temperatures are about  $0.8^\circ\text{C}$ . higher than those reported in Table II. Since there is only one degree of thermodynamic freedom along this line, the  $0.8^\circ\text{C}$ . higher temperature is equivalent to concentrations which are 0.04 mole fraction methane higher, and pressures which are approximately 3.5 atm. higher than those in Table II. It is highly likely that the Papahronis results are in error because the three-phase line does not extrapolate to the literature value of the triple point of pure *n*-octane but to a value  $0.7^\circ\text{C}$ . higher, and the heat of fusion of *n*-octane cannot be calculated accurately employing Papahronis data in the Van't Hoff isochore even in the low concentration methane region.

Figure 1 presents a temperature-composition diagram at 20 atm. pressure showing that the solid-vapor region cuts through the vapor-liquid region. The upper solid-liquid-vapor line is shown at  $-61.60^\circ\text{C}$ . and the lower solid-liquid-vapor line is shown at  $-107.60^\circ\text{C}$ . The vapor phase at these temperatures contains more than 0.999 mole fraction methane.

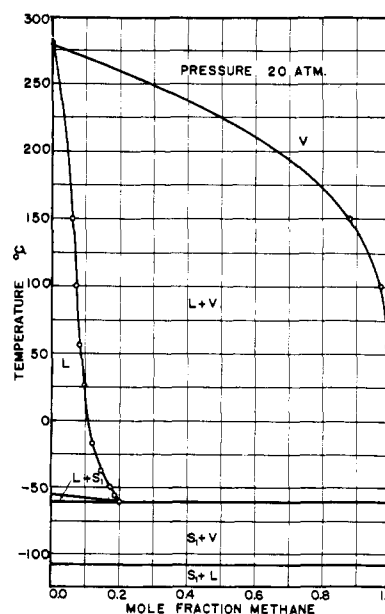


Figure 1. Isobaric temperature composition 20 atm. pressure

Figure 2 presents the fugacities of methane in solution in the low temperature range.

The fugacities of pure methane as given in Matthews (7) were used to compute the fugacities of the methane in solution at temperatures of  $25^\circ\text{C}$ . and lower. The calculation is valid since, at these low temperatures, the vapor state at all pressures studied was methane containing less than 0.001 mole fraction *n*-octane. Large scale graphs of fugacity of dissolved methane vs. composition in mole fraction were linear in the composition range below 0.20 mole

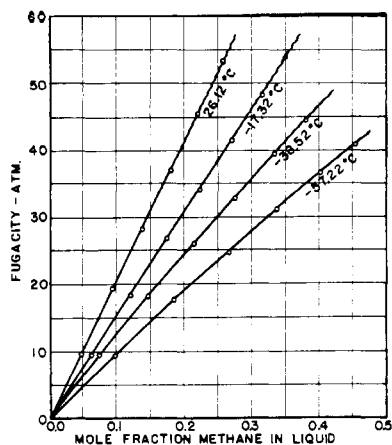


Figure 2. Fugacity of methane in *n*-octane

fraction methane. Thus methane in solution in *n*-octane at temperatures below 25° C. definitely follows Henry's law at concentrations up to 0.20 mole fraction methane.

The thermodynamic dependence of the Henry's law constant with temperature is given by:

$$\frac{d \ln f/x}{d(1/T)} = - \frac{(H_2^* - H_2)}{R}$$

The slopes of the lines of the large scale fugacity-composition diagram were plotted as logarithm of  $f/x$  vs. reciprocal absolute temperatures. The graph was a straight line indicating that the following thermodynamic simplifications are true at concentrations of methane to 0.20 mole fraction and from 25° C. to the freezing point of *n*-octane:

$$H_2^* = H_2(\text{gas}) = H_2(\text{gas})$$

$$H_2 = H_2$$

$$\Delta C_P = C_{P2}(\text{gas}) - \bar{C}_{P2} = 0$$

From the slope of the straight line the enthalpy change of methane on solution [ $H_2(\text{gas}) - H_2$ ] was

$$\Delta H = +1240 \pm 50 \text{ cal./gram mole}$$

The following thermodynamic properties of the methane-*n*-octane system in the temperature range -60 to 25° C. and in the composition range 0 to 0.20 mole fraction methane are accurate within the designated levels.

Thermodynamic Property	Function or Numerical Value, Cal./Gram Mole
$\Delta H = H_2(\text{gas}) - H_2$	$1240 \pm 50$
$\Delta S = S_2(\text{gas}) - \bar{S}_2$	$1240 \pm 50$
	$T$
$\Delta G = G_2(\text{gas}) - \bar{G}_2$	0
$\Delta C_P = C_{P2}(\text{gas}) - \bar{C}_{P2}$	0
$H_1(\text{liq}) - H_1(\text{solid})$	$4953 \pm 31$
$S_1(\text{liq.}) - S_1(\text{solid})$	$4953 \pm 31$
	$T$

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## NOMENCLATURE

- $C_{P2}(\text{gas})$  = molar heat of methane in the gas phase at any temperature and pressure, cal./gram mole  $\times$  ° K.  
 $\bar{C}_{P2}$  = partial molar heat capacity of methane in a liquid solution of any dilution, cal./gram mole  $\times$  ° K.  
 exp. = base of the Napierian logarithm system  
 $f$  = fugacity of methane (atm.)  
 $G$  = Gibbs free energy, cal./gram mole  
 $H_2^*$  = partial molar enthalpy of methane in the ideal gas state at  $T$ , cal./gram mole  
 $H_2^{\ddagger}$  = partial molar enthalpy of methane in an infinitely dilute solution at  $T$ , cal./gram mole  
 $H_2$  = partial molar enthalpy of methane in a liquid solution of any dilution at  $T$ , cal./gram mole  
 $H_2(\text{gas})$  = molar enthalpy of methane in the gas phase any  $T$  and  $P$ , cal./gram mole  
 $L$  = liquid phase  
 $P_1$  = normal vapor pressure of *n*-octane at  $T$ , atm.  
 $P$  = total pressure of the system, atm.  
 $P_r$  = reduced pressure of *n*-octane  
 $R$  = universal gas constant  
 $S_1$  = solid *n*-octane phase, molar entropy of *n*-octane, cal./gram mole  $\times$  ° K.  
 $T$  = absolute temperature of system, ° K.  
 $T_r$  = reduced temperature of *n*-octane  
 $V$  = vapor phase; molar volume of liquid, ml./gram mole  
 $x_1$  = mole fraction *n*-octane in the liquid phase  
 $y_1$  = mole fraction *n*-octane in the gas phase  
 $\gamma_1$  = activity coefficient of *n*-octane in the liquid phase  
 $\nu_{P1}$  = fugacity coefficient of *n*-octane in the liquid phase at the normal vapor pressure of *n*-hexane at  $T$   
 $\nu_P$  = fugacity coefficient of *n*-octane in the gas phase at the total pressure of the system at  $T$

The standard state of the solute is the hypothetical incompressible liquid of unit mole fraction obeying Henry's law. The standard state of the solvent is the pure liquid under its own vapor pressure.

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